



# Recovery of phosphorus by chemical treatment

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## Relevant research question:

What about the saturated adsorption material: should it simply be disposed of as solid waste? When is recovery/regeneration recommended?

## P-recovery?

- The main objectives:
  - **Regeneration of the saturated sorbents** making it reusable in several adsorption/desorption cycles and
  - **Recovery of phosphorus** by precipitation or used directly with irrigation water as fertilizer
- The reusability of the granules is as important (or even more) than recovering phosphate
- A desorption process using an **alkaline** solution is proposed without harming the adsorbing material.



**Integration of P-adsorbing material in a circular process**

**Iron Coated Sand (ICS)**

**DiaPure®**

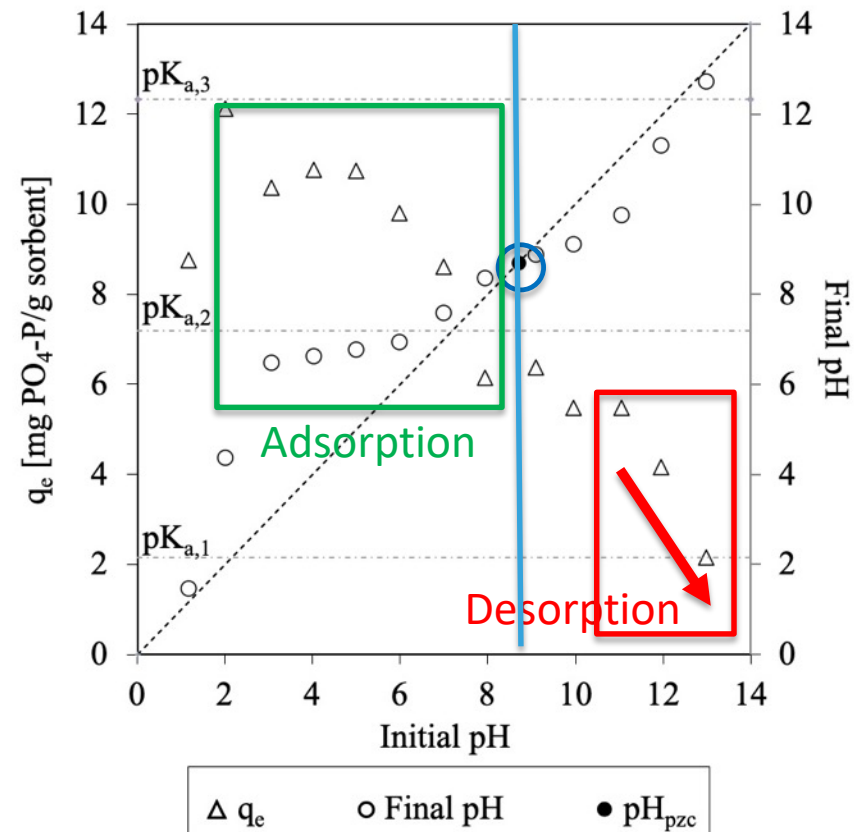
**Vito A & B**

**FerroSorb SW**

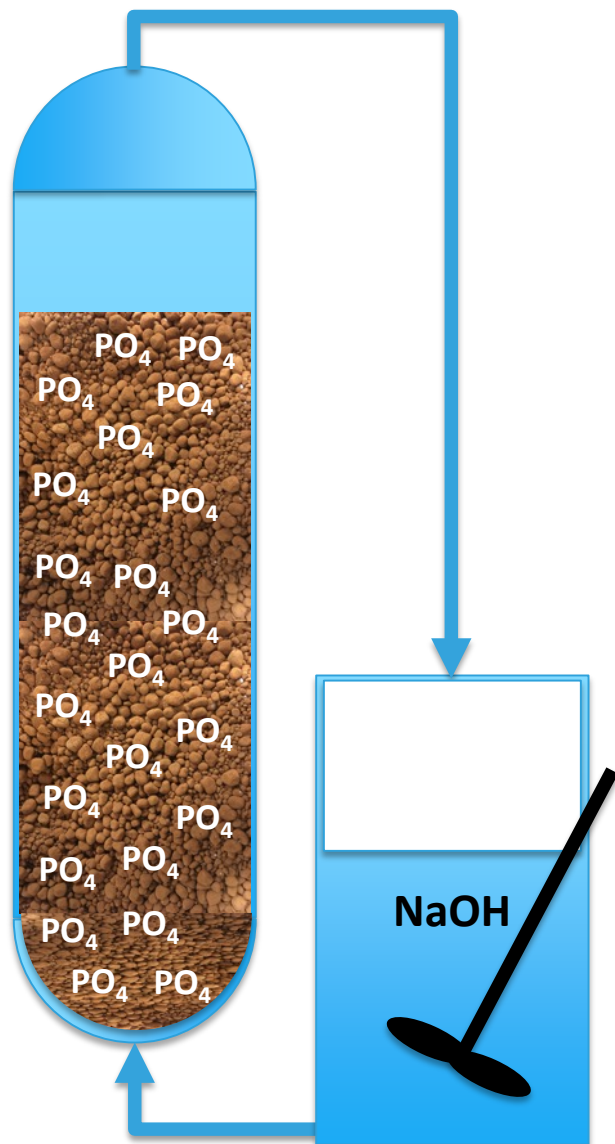
# Introduction

## Theoretical basis:

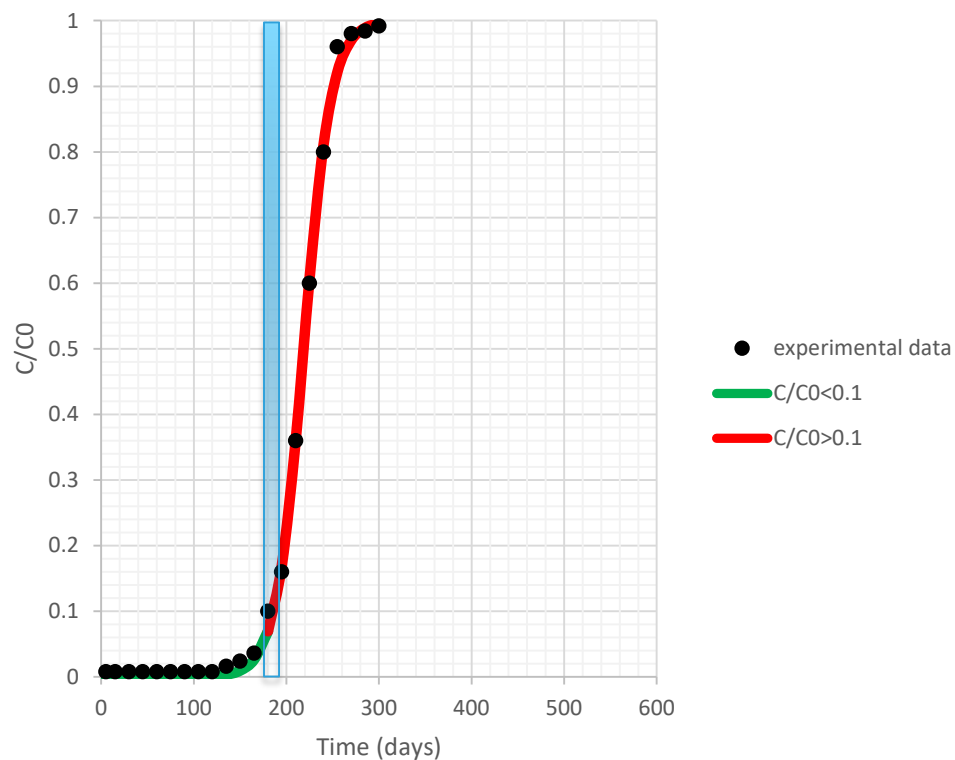
- The influence of initial pH on the adsorption capacity  $q_e$  for Fe and Al based adsorption materials
  - Adsorption/desorption are **balancing processes** until an equilibrium is reached!
- 
- pH 8.7 =  $\text{pH}_{\text{PZC}}$   
= final pH is equal to the initial pH
  - pH range 2 - 8.7: high  $q_e$
  - pH range 8.7 – 13: low  $q_e$
  - pH > 11 the  $q_e$  drops considerably



# Concept of alkaline desorption

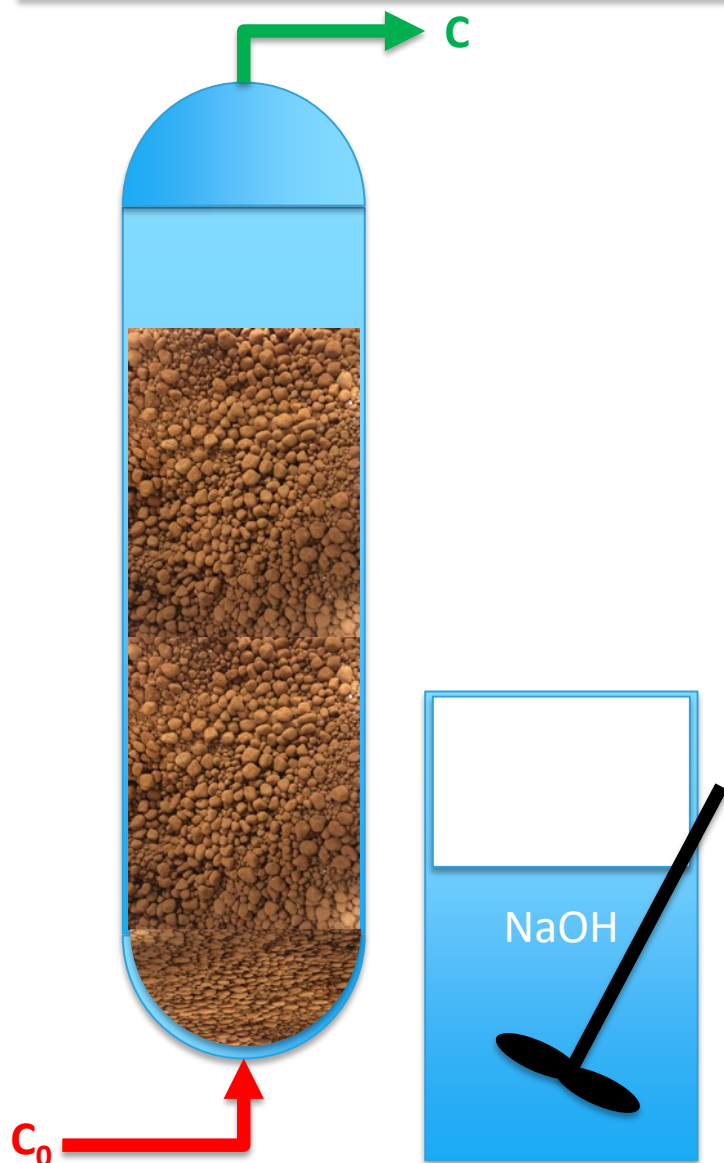


## Desorption Phase @ $C/C_0 = 0.1$



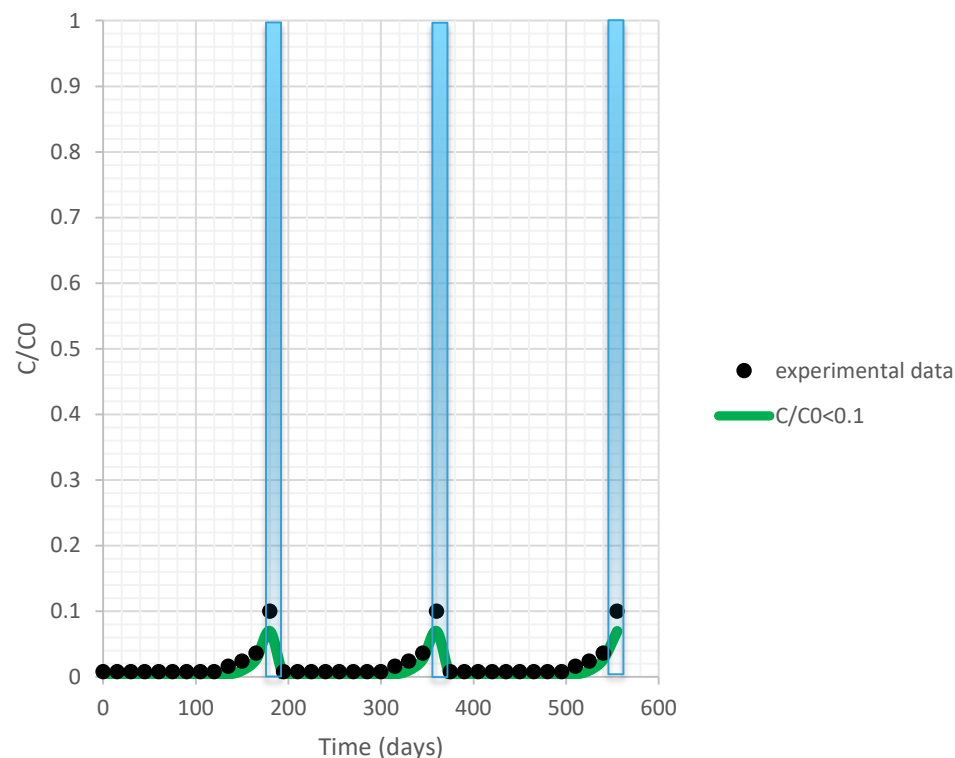


# Concept of alkaline desorption



Regeneration of the saturated sorbent and recovery of phosphorus

Intermittent regeneration of ICS



# Materials & Methods

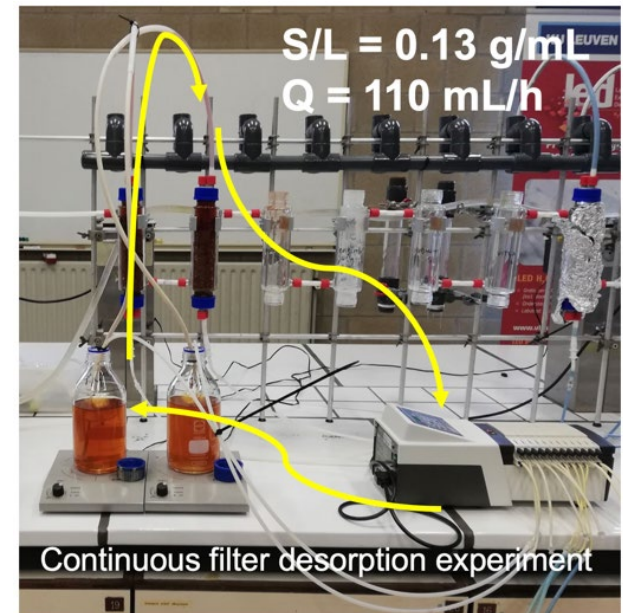
1. **Batch desorption experiments:** 5g of pre-dried saturated ICS was brought into contact with NaOH solution.

Variable parameters:

- NaOH concentration (1-0.5-0.1- 0.01- 0.001M),
- Desorption time (5min-48h)
- Solid/liquid ratio (S/L= 0.03-1 g/mL)

2. **Continuous filter ad- & desorption experiments:** 1 liter of NaOH solution was recirculated over an adsorption column filled with 150 cm<sup>3</sup> of saturated adsorption material.

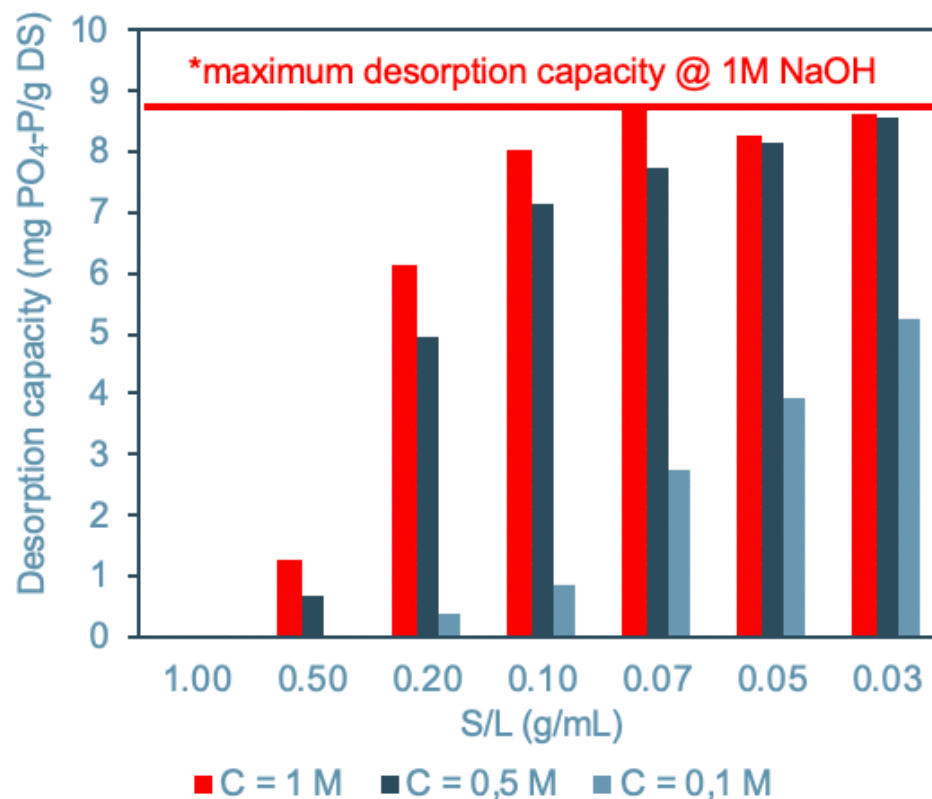
3. **Analysis of the samples:** **Liquids:** PO<sub>4</sub>-P determination by ion chromatography after .45 µm filtration. **Solid granules:** SEM-EDX.



# Results & Discussion

## Batch experiments

- The composition of 1 g of saturated ICS granules was determined by a complete destruction of the granules by Aqua Regia and ICP analysis:
  - Phosphorus: 15.30 +/-1.25 mg P/g DS **=1.5%P**
  - Iron: 590.7 +/-8.7 mg Fe/g DS **=59%Fe**
- Optimal NaOH concentration = 0.5 M
- Optimal contact time = 24 h or more
- Optimal S/L ratio = 0.10 - 0.05 g/mL
- P-desorption efficiency > 50% @ 0.5 and 1 M NaOH



# Results & Discussion

## Continuous filter experiments: Adsorption

- The breakthrough curve of ICS column experiments with an Empty Bed Contact Time (EBCT) of 5.5 h and 0.5 h results in a breakthrough time of 180 days and 7 days respectively.

Regeneration is highly appropriate in the case of a short EBCT

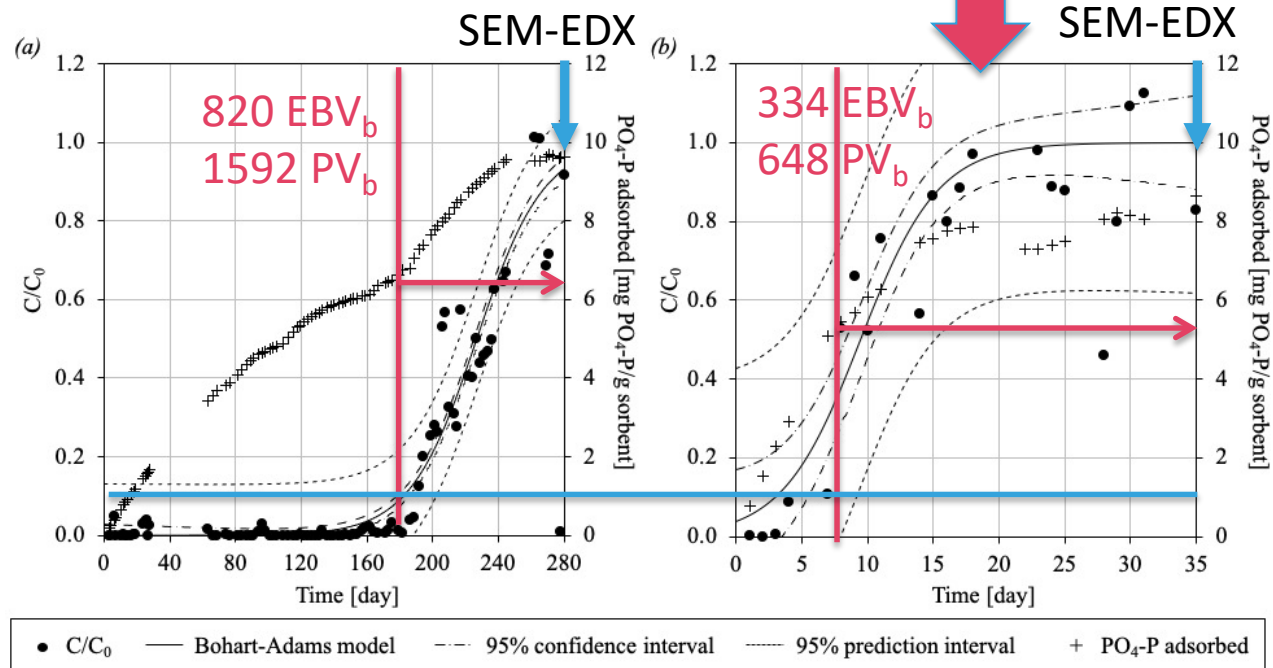
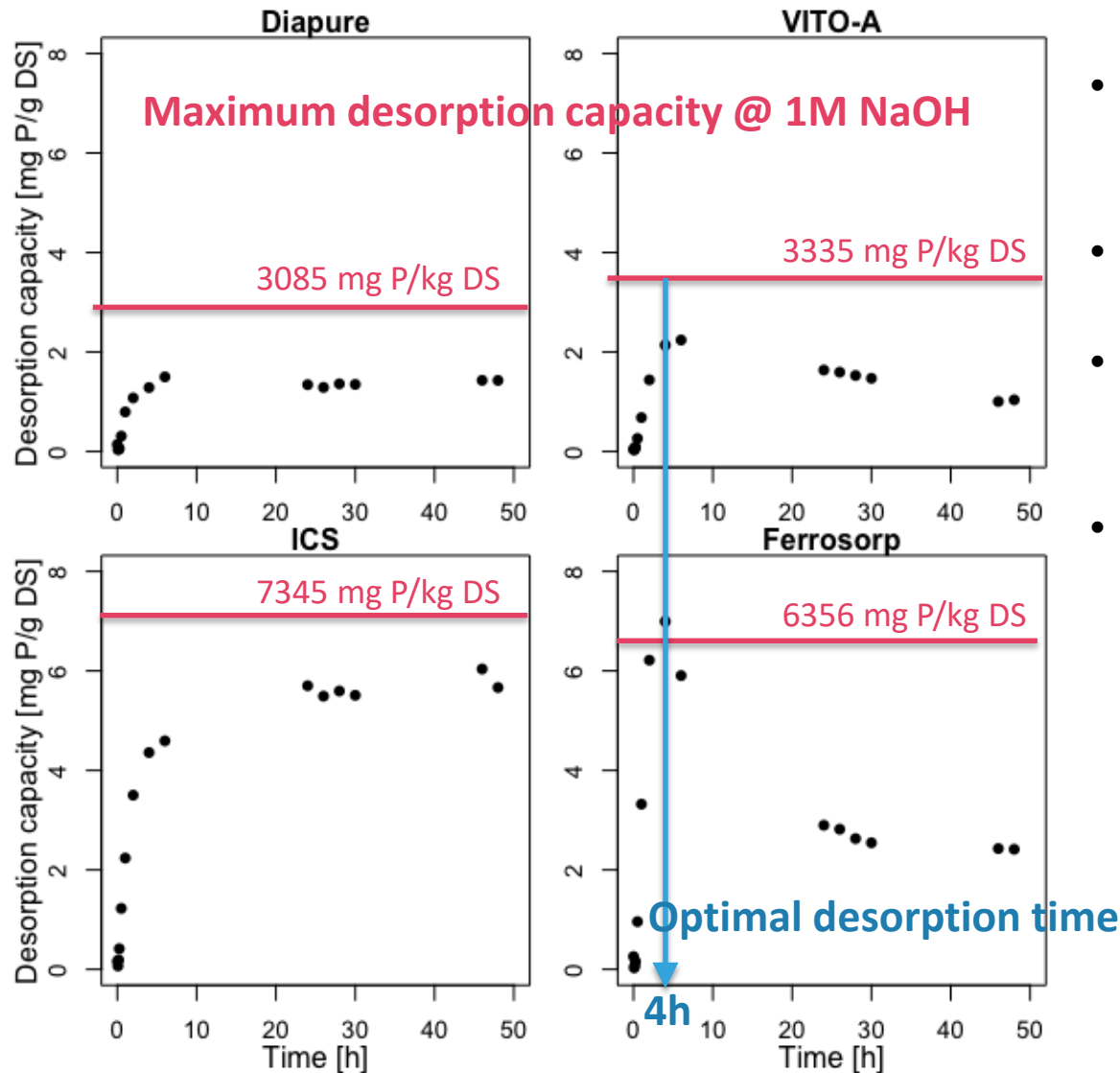


Figure: ICS adsorption column experiments on lab-scale (influent P concentration = 25 mg PO<sub>4</sub>-P/L) with EBCT= 5.5 h (a) and EBCT= 0.5 h (b)

# Results & Discussion

## Continuous filter experiments: Desorption



- Continuous desorption experiment in recycle
- NaOH concentration = 0.5 M
- Optimal desorption time = material dependent
- P-desorption efficiency > 50% @ 0.5 NaOH



# Results & Discussion

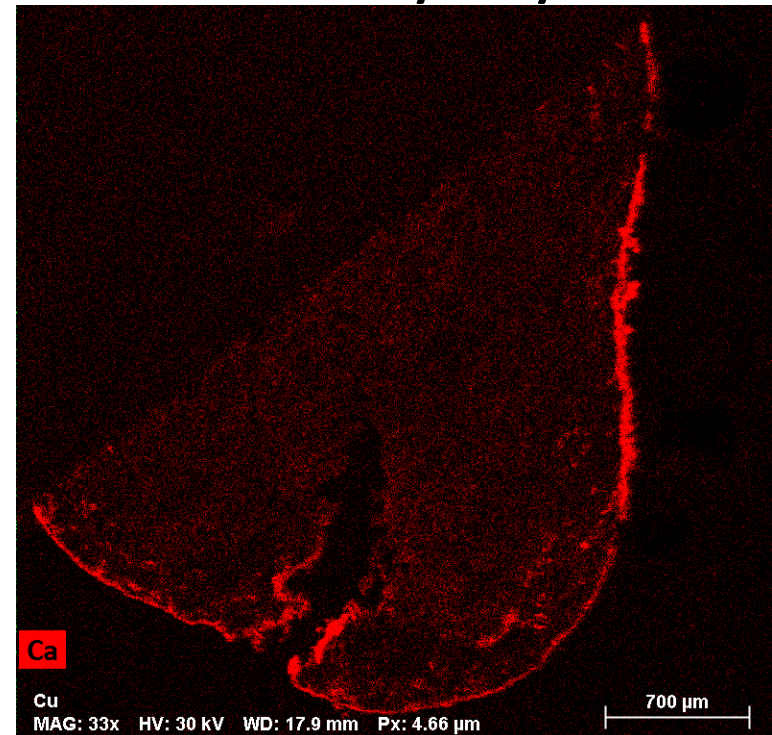
## SEM-EDX analysis @ EBCT of 0.5 h

- SEM-EDX of saturated DiaPure® of column experiment with **EBCT of 0.5 h**.
  - The phosphate is mainly adsorbed at the outer layers of granules.
  - Calcium forms deposits on the adsorbent surface and disturb the alkaline desorption.
  - Acid regeneration step before alkaline desorption?

polished **DiaPure®** granule  
embedded in a resin



Fe – P – Ca analysis by EDX

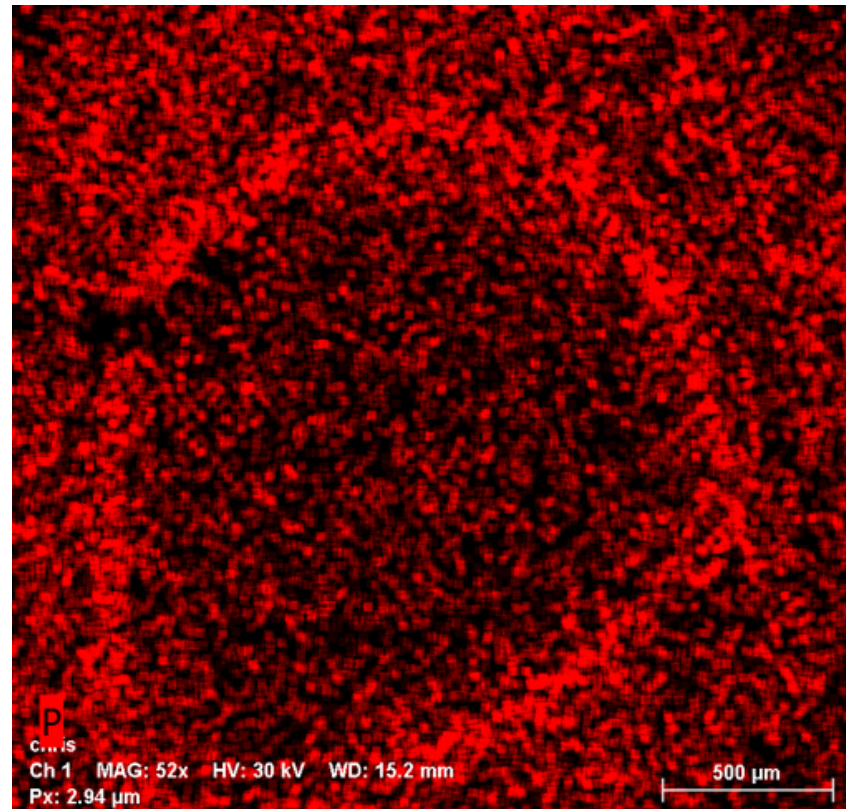


# Results & Discussion

## SEM-EDX analysis @ EBCT of 5.5 h

- SEM-EDX of saturated ICS of column experiment with **EBCT of 5.5 h**.
  - Phosphorous is accumulated at the sand core of the granule.
  - Phosphorous migrates towards the core of the granule.

Si – Fe – P analysis by EDX



# Conclusions

- Optimal NaOH concentration = 0.5 M
- Optimal desorption contact time = material dependent
- P-desorption efficiency > 50% @ 0.5 M NaOH
- Leaching of Fe during the desorption process is a problem
- Desorption of P from the inner layers of the granule will be difficult
- Calcium deposits should be avoided by an acid wash





# Q & A



# Part IV: Nutrient removal modelling

# Nutrient reduction potential using end-of-pipe solutions for an entire catchment

Andreas Bauwe, Bernd Lennartz – University of Rostock

#EUGreenWeek

2021 Partner Event

+++ Filter systems for nutrient removal from agricultural waters +++

1 June 2021

# The Warnow river basin

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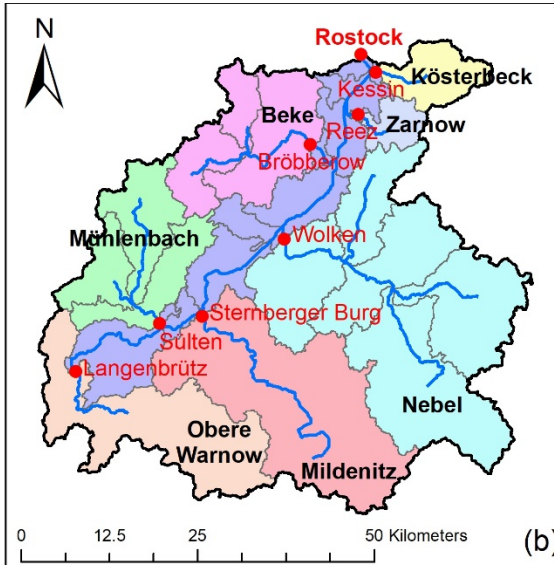


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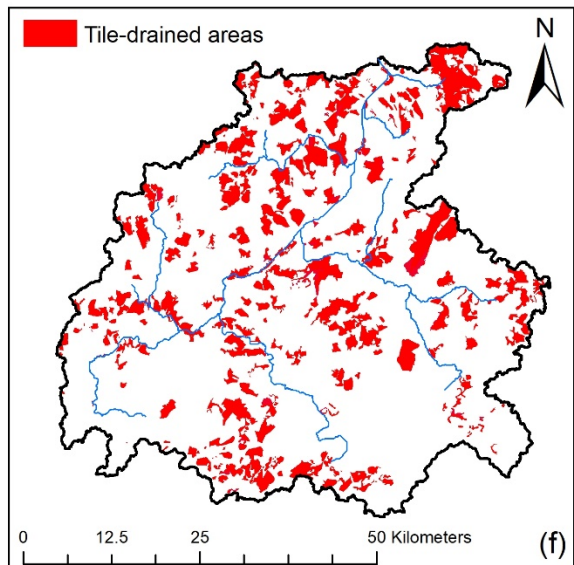
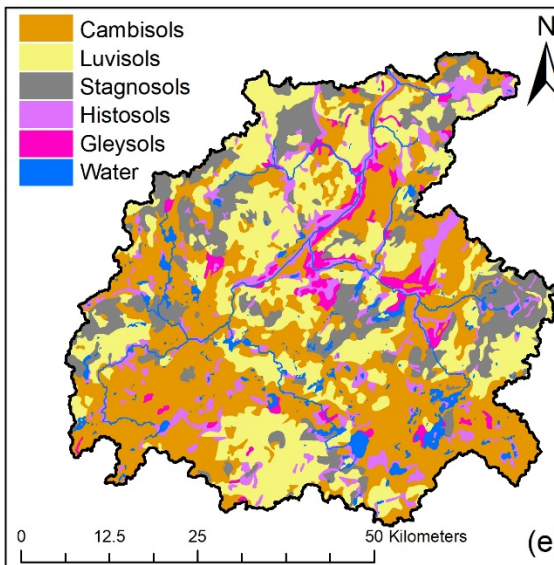
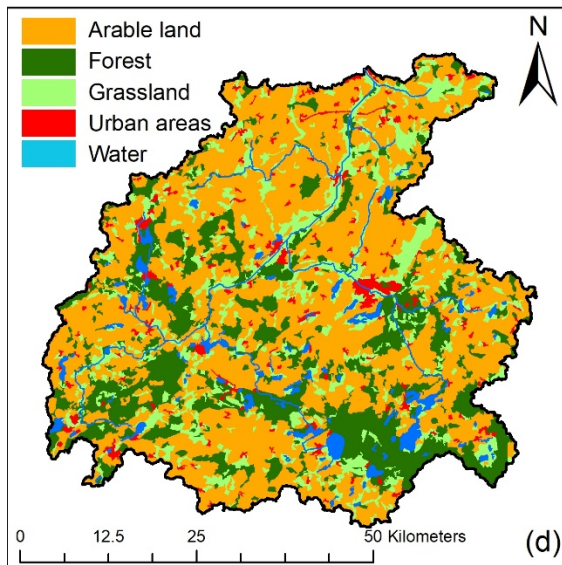


Size: ca. 3,000 km<sup>2</sup> (second largest German watershed that discharges into the Baltic Sea)

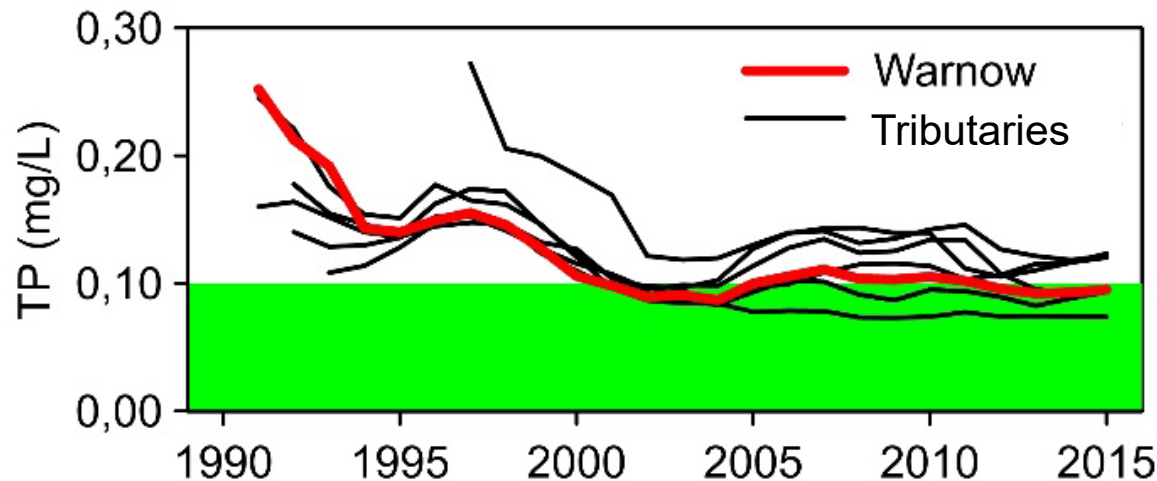
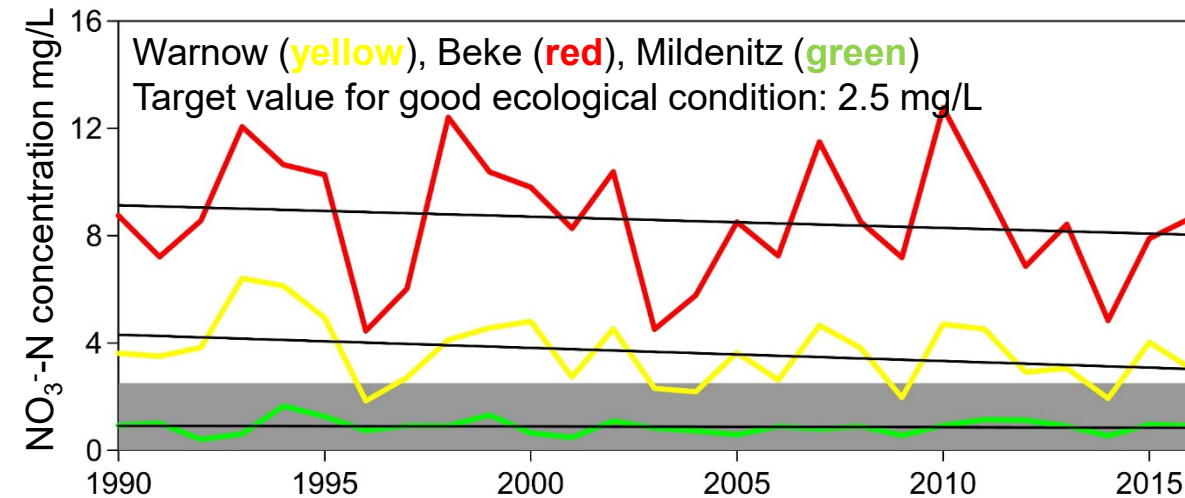
Land use: Arable land (57%), Forest (21%), Pasture (15%)

Soils: Cambisols, Luvisols

Tile-drained areas: 19%



# Background



- Slow decrease of NO<sub>3</sub><sup>-</sup>-N concentrations during the last 30 years
- Large differences in NO<sub>3</sub><sup>-</sup>-N concentrations among the sub-basins depending on land use
- Mitigation measures needed for sub-basins dominated by agriculture
- Strong decrease of TP concentrations in the early 1990s mainly due to improved treatment of wastewater
- Target values for TP are complied in most sub-watersheds
- However: HELCOM demands a reduction 110 t TP/a for Germany



Reduction measures  
needed for N + P  
(end-of-pipe)

End-of-pipe solutions to reduce nutrient loads  
in tile-drained areas

**Phosphorus  
Filters**

**Nitrogen  
Constructed wetlands**

Modeling the reduction potential  
using the SWAT model

Model input

- Digital Elevation model,
- Weather data
- Land use
- Soil data
- Land management
- Vegetation
- ....

Modelling approach

1. Calibration and validation of stream flow
2. Calibration and validation of P and N loadings
3. Implementation of filters and constructed wetlands in the model

# Reference simulation

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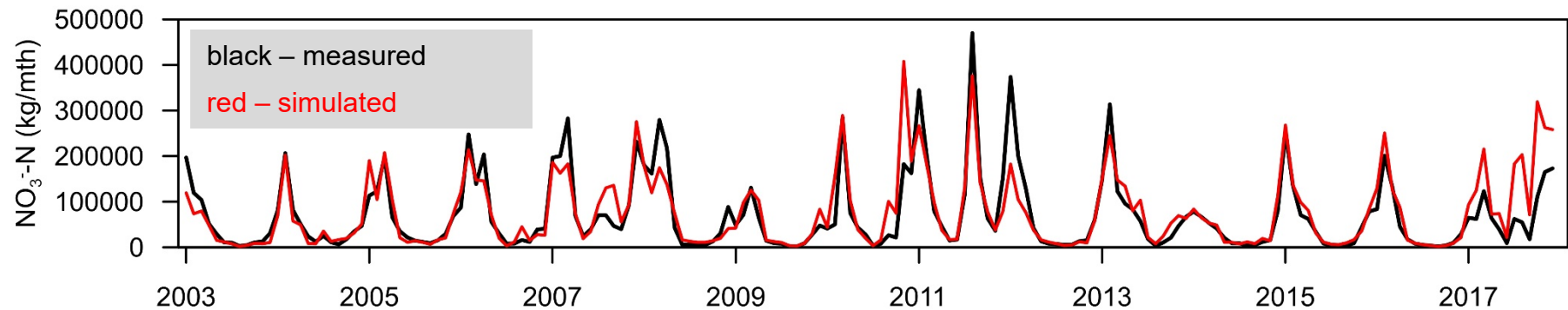
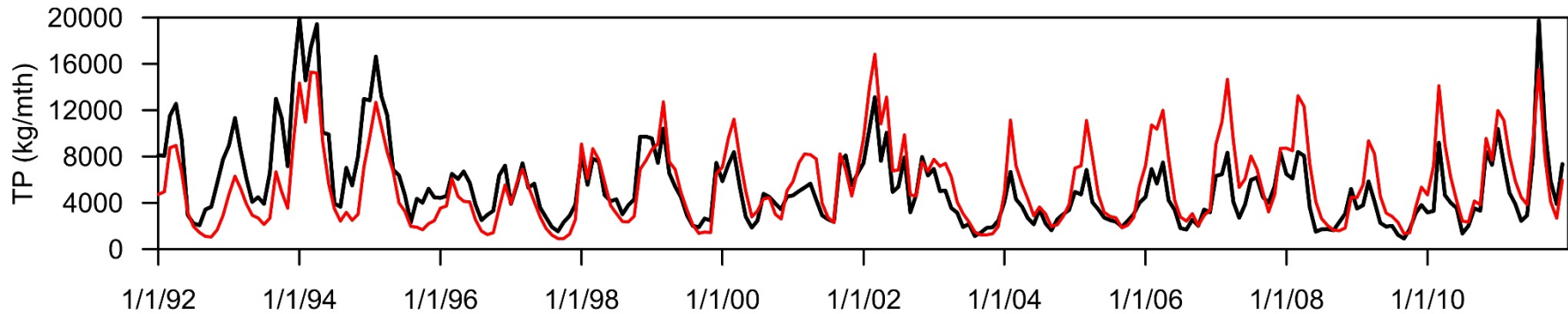
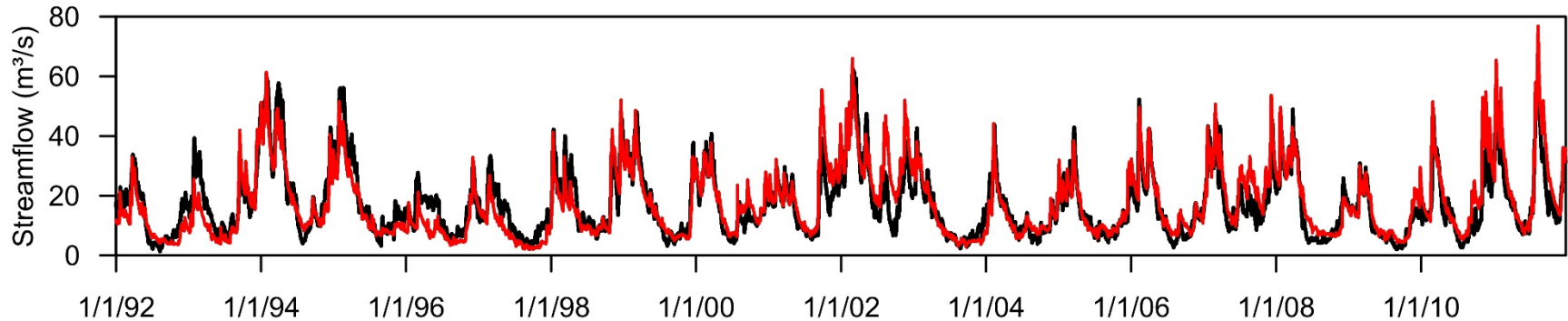


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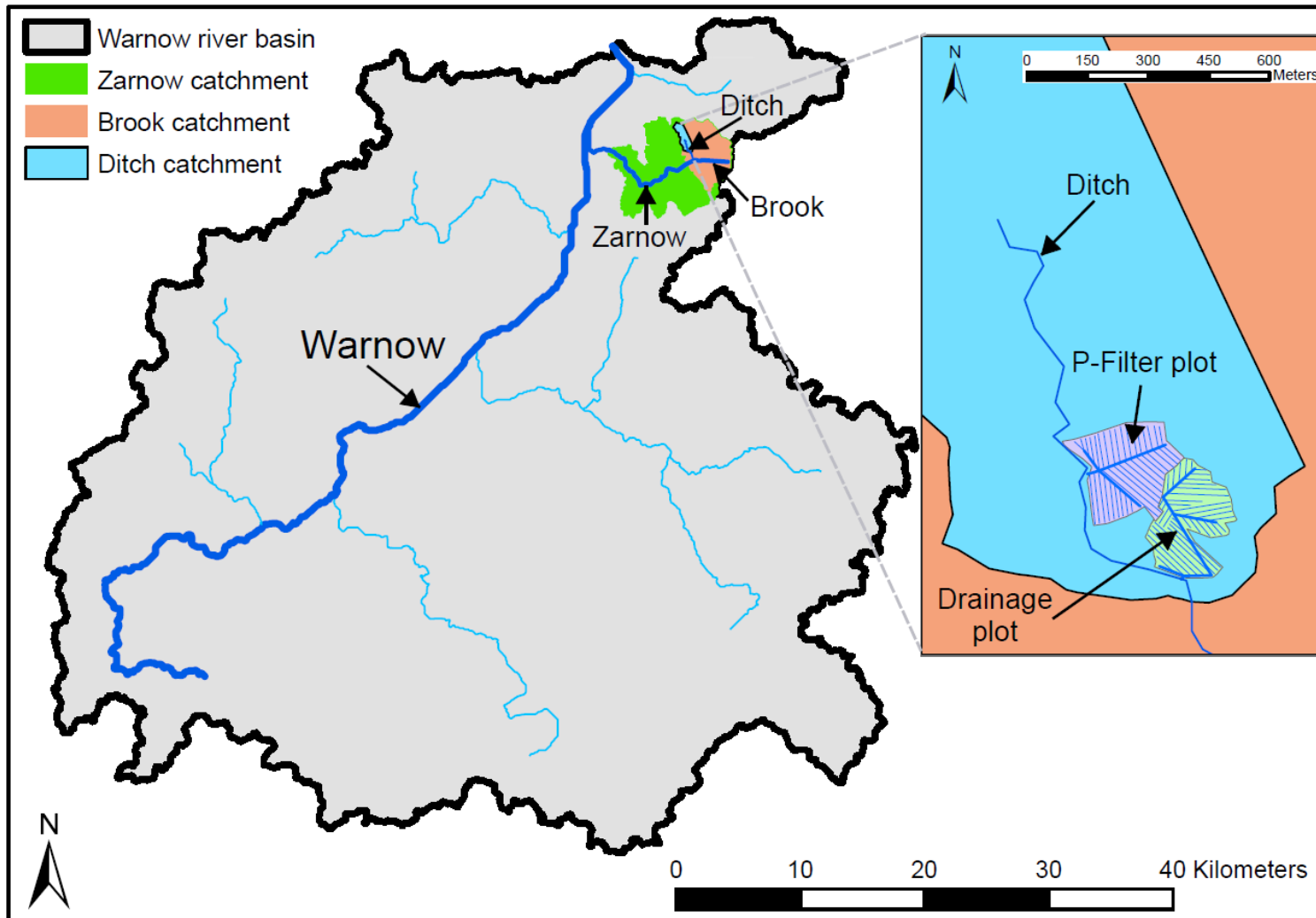


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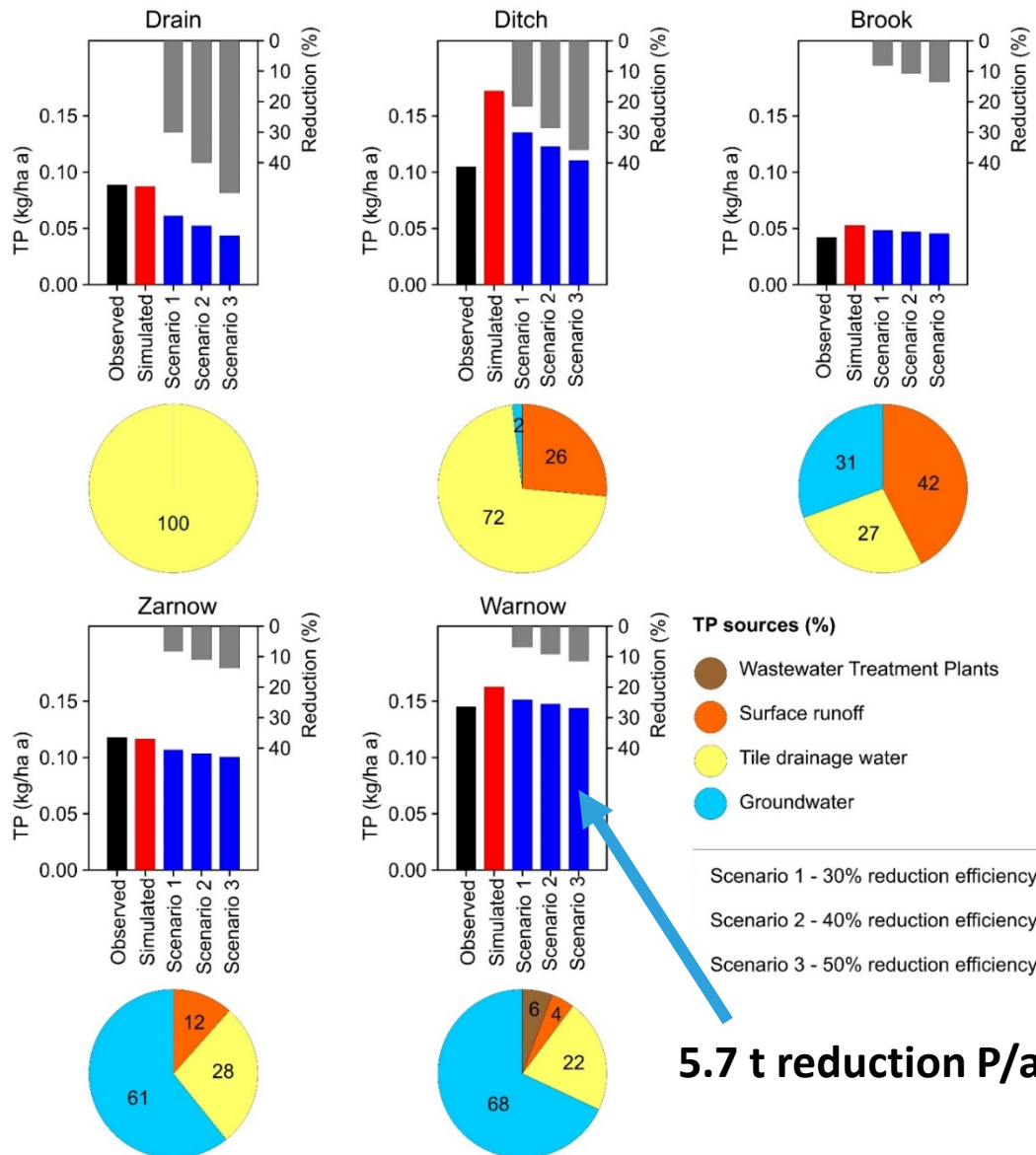


## Evaluation of P filters in tile-drained areas at different spatial scales



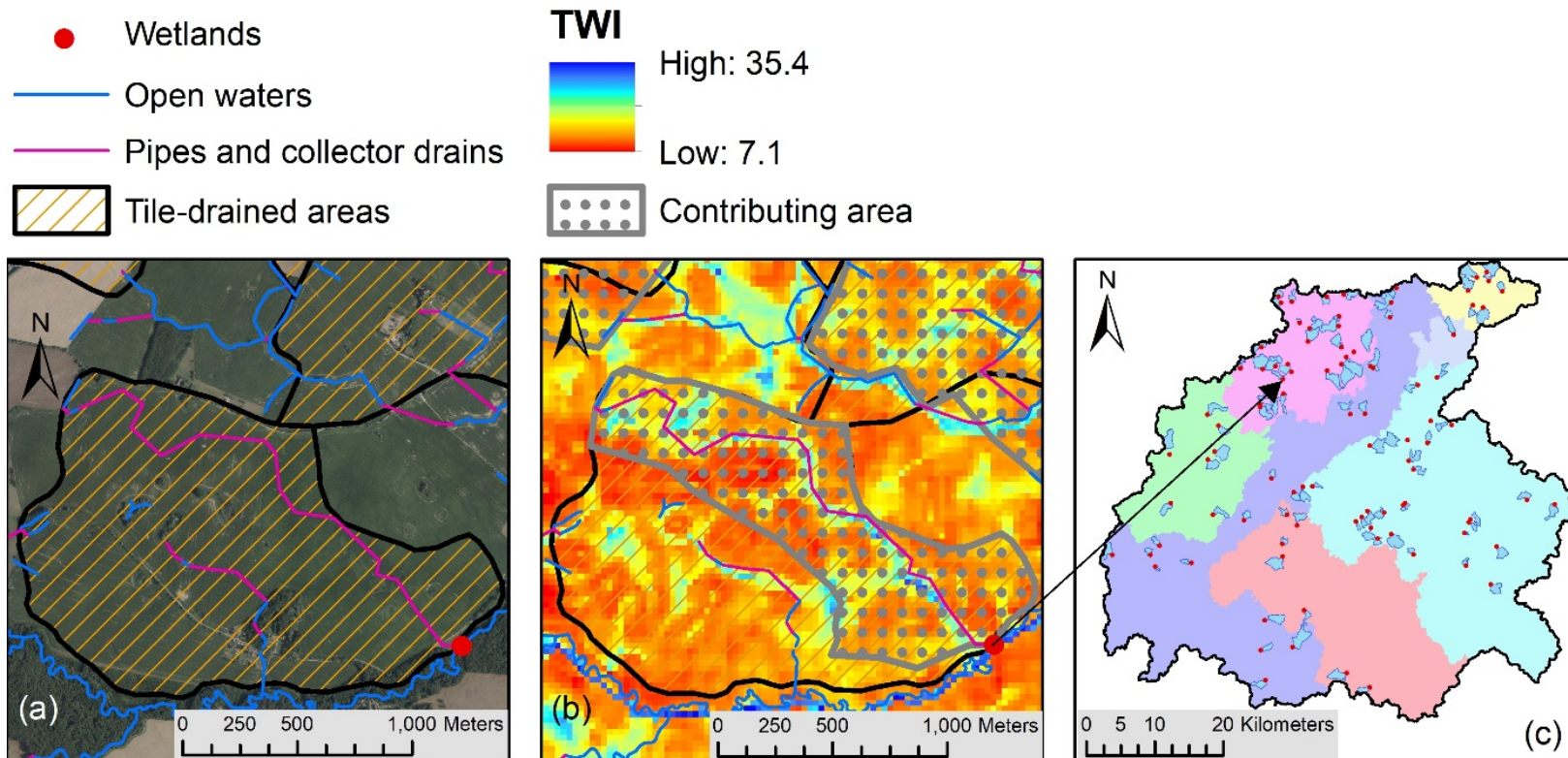


# P reduction scenarios



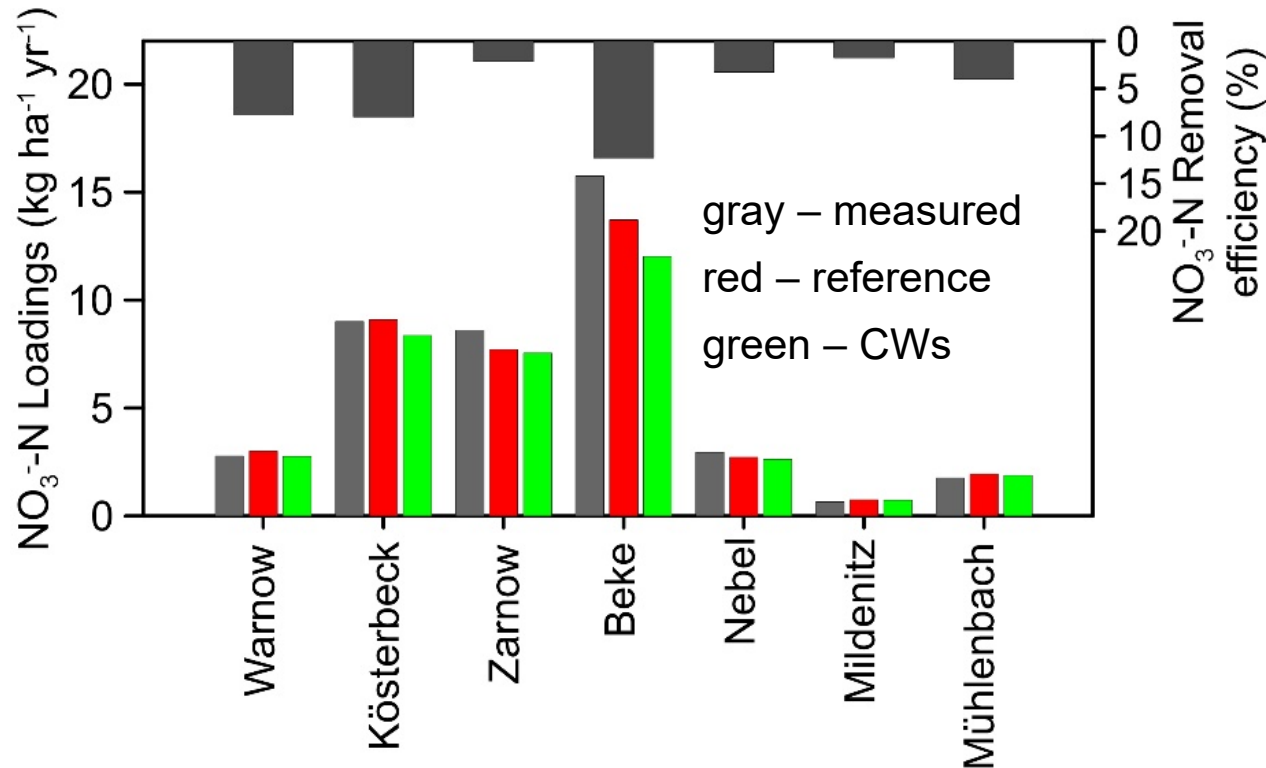
- Good fit of measured and modeled values at different spatial scales.
- Effect of P filters at catchment scale depends on proportion of tile-drained areas.
- P filters could contribute to reduce P losses notably in the Warnow river basin.

## Evaluation of constructed wetlands in tile-drained areas



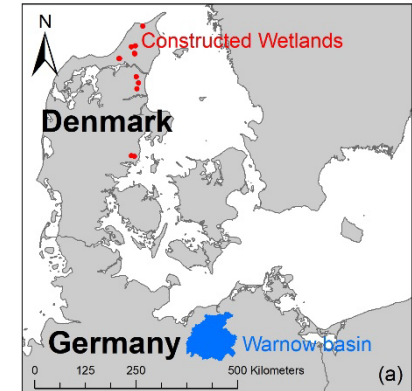
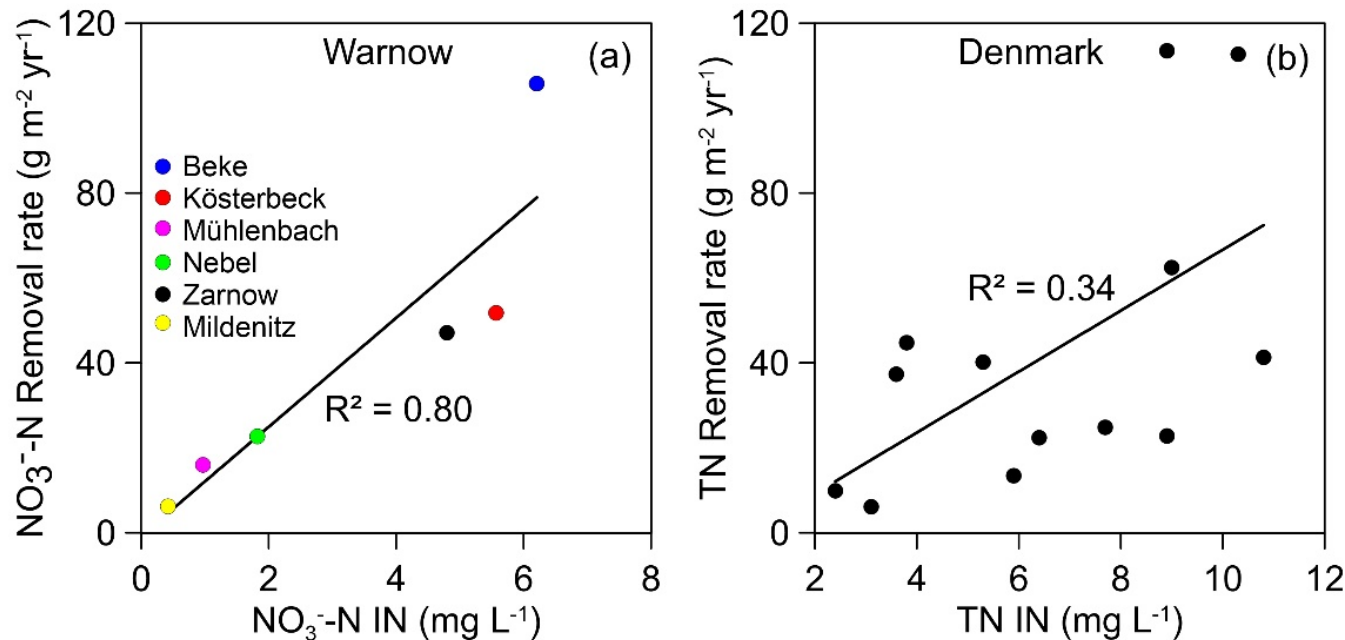
- Contributing areas were identified by using maps of tile-drained areas, running waters (open or as pipes) and aerial photographs.
- Constructed wetlands (CWs) were placed in moist areas according to topographic wetness index (TWI).
- 97 suitable spots for CWs were identified.

# N reduction scenarios



- Measured NO<sub>3</sub>-N loadings were reproduced well by the model.
- The implementation of constructed wetlands had positive effects on the surface water quality with an overall NO<sub>3</sub>-N removal efficiency of 7.8%.
- The NO<sub>3</sub>-N removal efficiency depended on subbasin characteristics (number of CWs, ratio between contributing area and subbasin area).

# N reduction scenarios



- The scenario results were verified by comparing simulation data with recordings of 13 existing CWs in Denmark (thanks to the Danish partners for providing the data!).
- The  $\text{NO}_3\text{-N}$  removal rates for the Warnow basin and CWs in Denmark were similar.
- Both for the Warnow basin and the CWs in Denmark, there was a significant positive relationship between input concentration and removal rate.
- Due to site-specific characteristics, this relationship was weaker for the Danish CWs.

- Through the widespread installation of filters in tile-drained areas, the **TP loads** in surface waters could be reduced by  $5.7 \text{ t yr}^{-1}$ , which corresponds to an overall reduction of ca. **10%**.
- The effect of P filters on a catchment scale depends on proportion of tile-drained areas.
- **NO<sub>3</sub><sup>-</sup>-N loads** could be reduced from  $900 \text{ t yr}^{-1}$  to  $840 \text{ t yr}^{-1}$ , which corresponds to an overall reduction of ca. **8%**.
- NO<sub>3</sub><sup>-</sup>-N removal rates varied strongly among the subbasins ranging from  $6$  to  $106 \text{ g m}^{-2} \text{ yr}^{-1}$  and they were positively correlated with the input concentrations.
- The installation of filters for P reduction and constructed wetlands for N reduction should be prioritized, focusing on hot-spot areas, in which the largest benefit is expected.



# Thank you!

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# Cost-effectiveness of the filters and the farmers' opinion

Charlotte Boeckert, Vlakwa



# P removal

## Drainage water

### P filterbox



80 – 100%

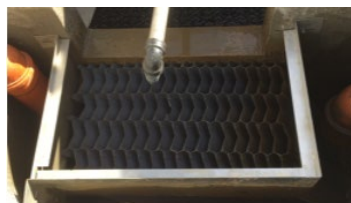
### Inline P filter



Organic matter

50 – 80%

### Sediment + reactive P filter



Sediments

ongoing

**0,1 – 0,5 mg P/l**

## Greenhouse effluent

### DIY



99%

### Company



99%

**10 – 20 mg P/l**



# Cost P filter

Water	Filter	CAPEX	OPEX	Yearly cost	Total P removal (kg P)	Cost effectiveness (€/kg P)
<b>Drainage (0,25 mg P/l)</b>	P filterbox	€ 635	€ 19	€ 78,2	0,06	<b>1 264</b>
	Drainage water (0,46 mg P/l)				0,19	409
	Drainagewater (0,12 mg P/l)				0,02	4 938
<b>Greenhouse (15 mg P/l)</b>	DIY	€ 690	€ 95	€ 164	1,94	<b>85</b>

# Cost effectiveness P-filter

## FL – Measures Cost Model

Measure	€/kg P
DIY	85
Non-turning soil tillage	174
Green cover	284
Municipal WWTP	363 - 1006
P filterbox	1264
Buffer strips	2160
Individual WWTP	5235 - 5913

# N removal

## Drainage water

### MBBR Subsoil



60%

### MBBR Containerized



75%

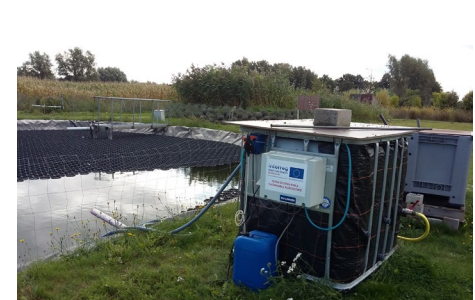
### ZVI



90%

## Greenhouse effluent

### DIY



85%

10 – 40 mg N/l

50 – 100 mg N/l

# Cost N filter

	Application	CAPEX	OPEX	Yearly cost	Total N removal (kg P)	Cost effectiveness (€/kg N)
DIY	Greenhouse effluent	€ 2 700	€ 1 400	€ 1 600	12.44	128.76
Subsoil	Drainage	€ 30 000	€ 2 900	€ 5 550	52.84	105.06
Containerized	Drainage Off-grid	€ 50 000	€ 2 700	€ 7 180	71.11	101.01
	Drainage	€ 40 900	€ 3 800	€ 7 460	71.11	104.97

# Cost effectiveness N-filter

## FL – Measures Cost Model

Measure	€/kg P
Green cover	3
Municipal WWTP	59(-163)
Reduced fertilization	70
MBBR	101-129
Individual WWTP	378-427

# Farmey Survey – FL - Greenhouses

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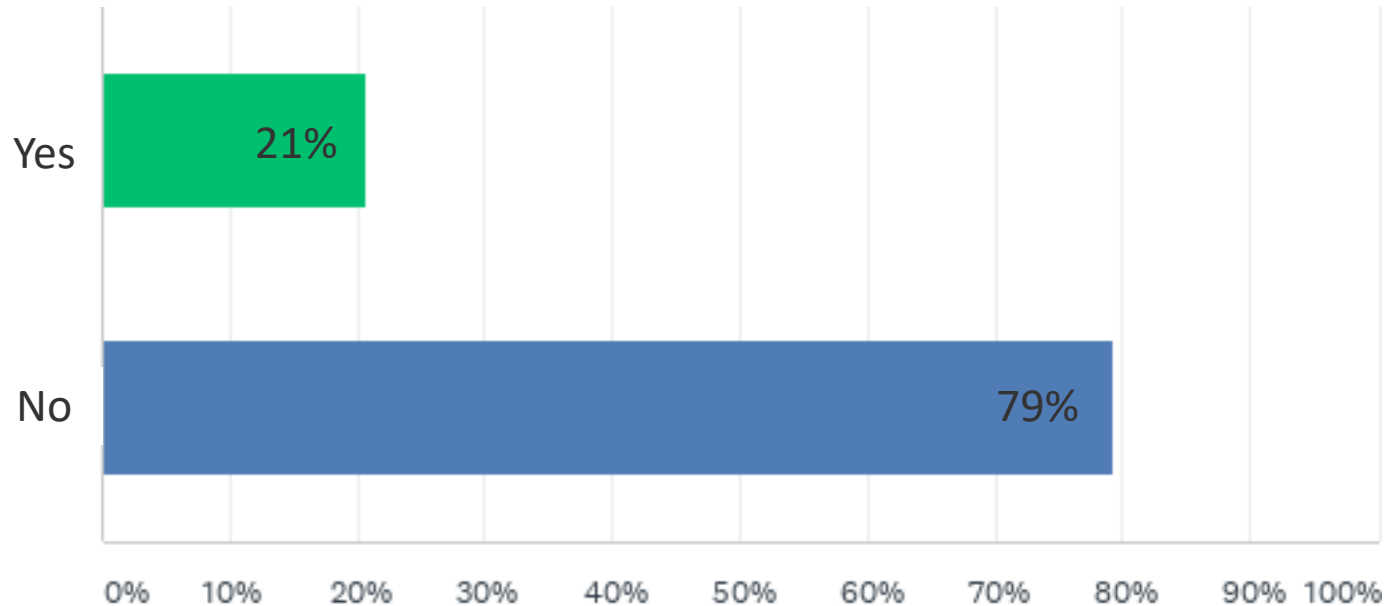
- Which requirements should the filter have?
- Are individual or collective filters recommended?
- Who should pay for these filters?



29 answers

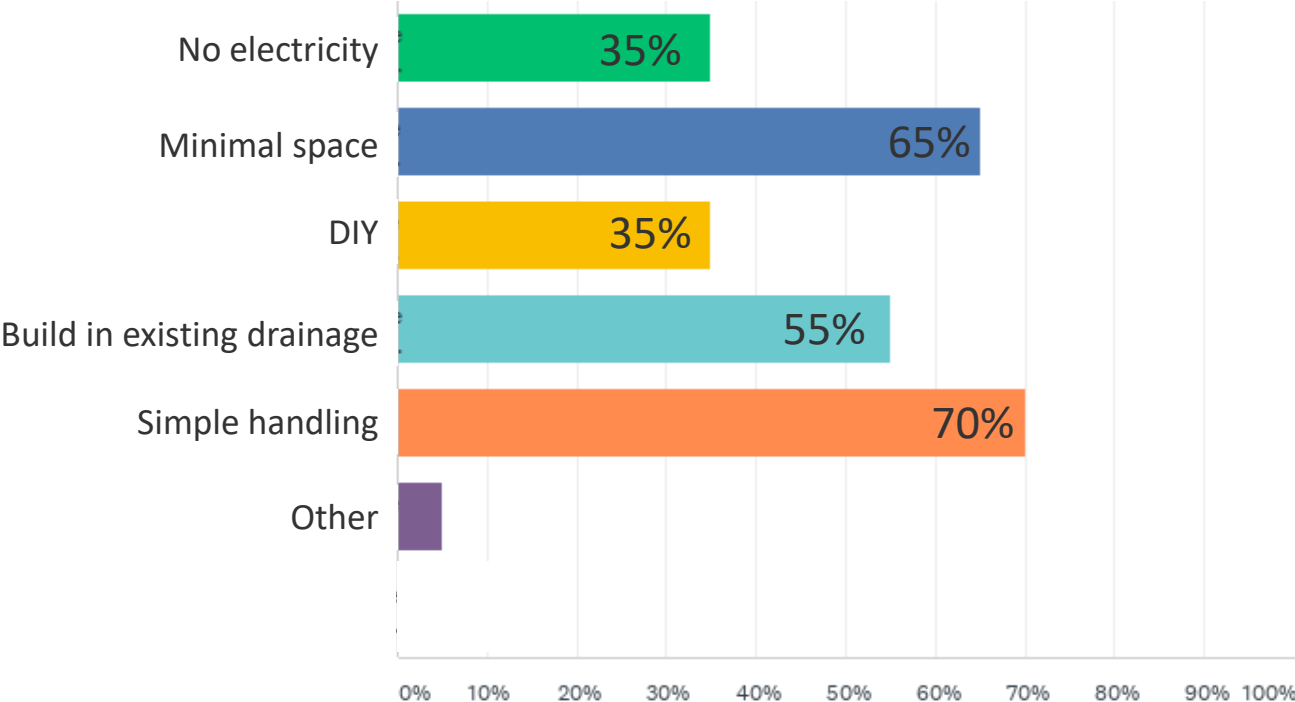
# Are you familiar with end-of-pipe technology to remove nutrients from agricultural waters?

Beantwoord: 29 Overgeslagen: 0



# Preferential requirements for the filter are:

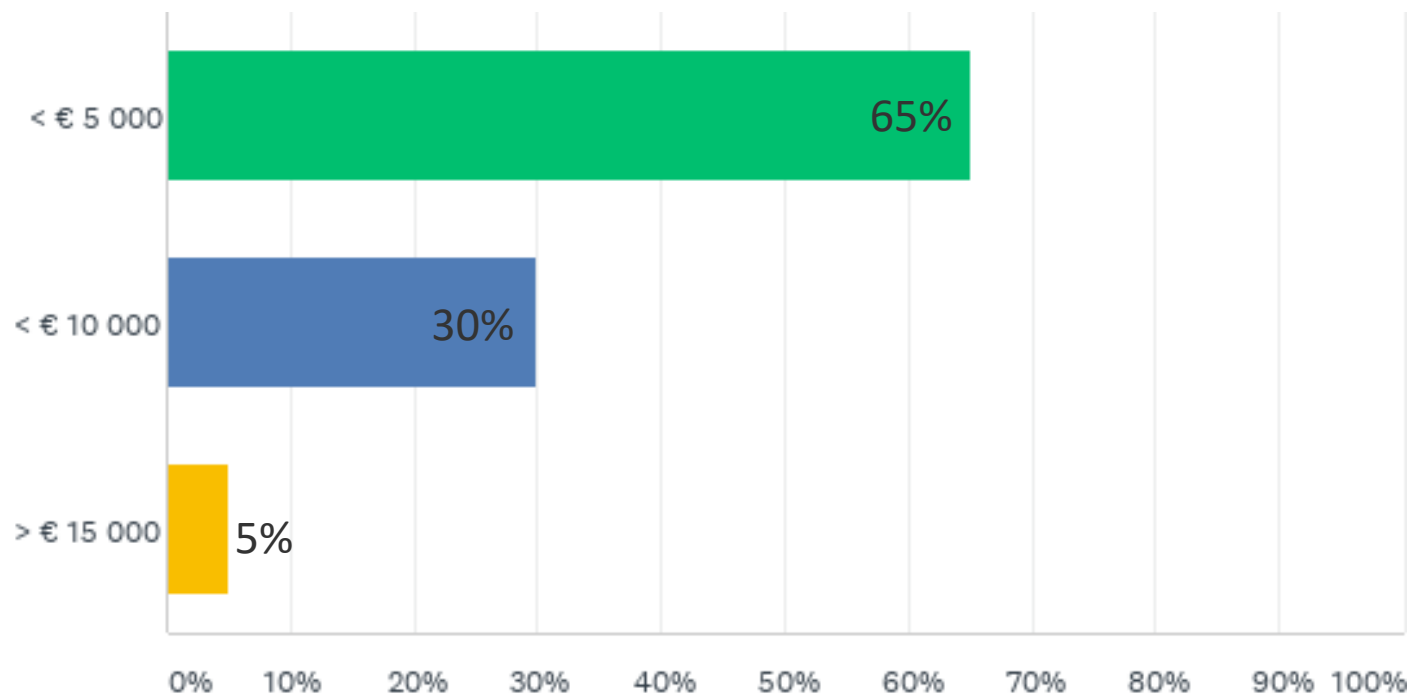
Beantwoord: 20 Overgeslagen: 9





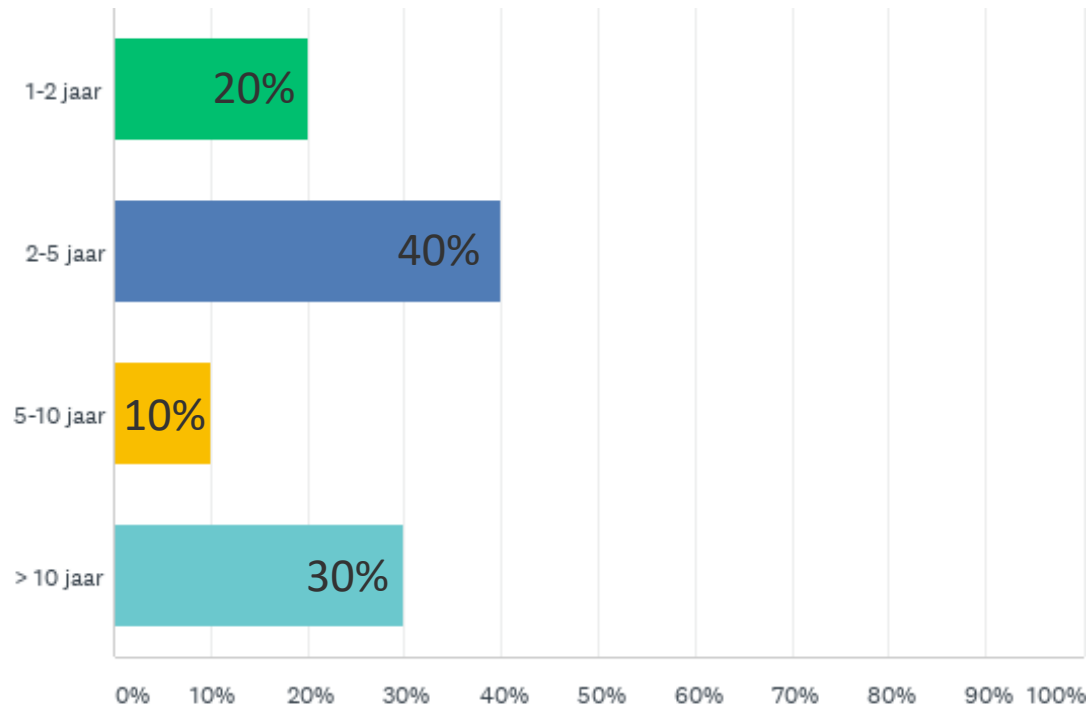
# Which investment cost is acceptable?

Beantwoord: 20 Overgeslagen: 9



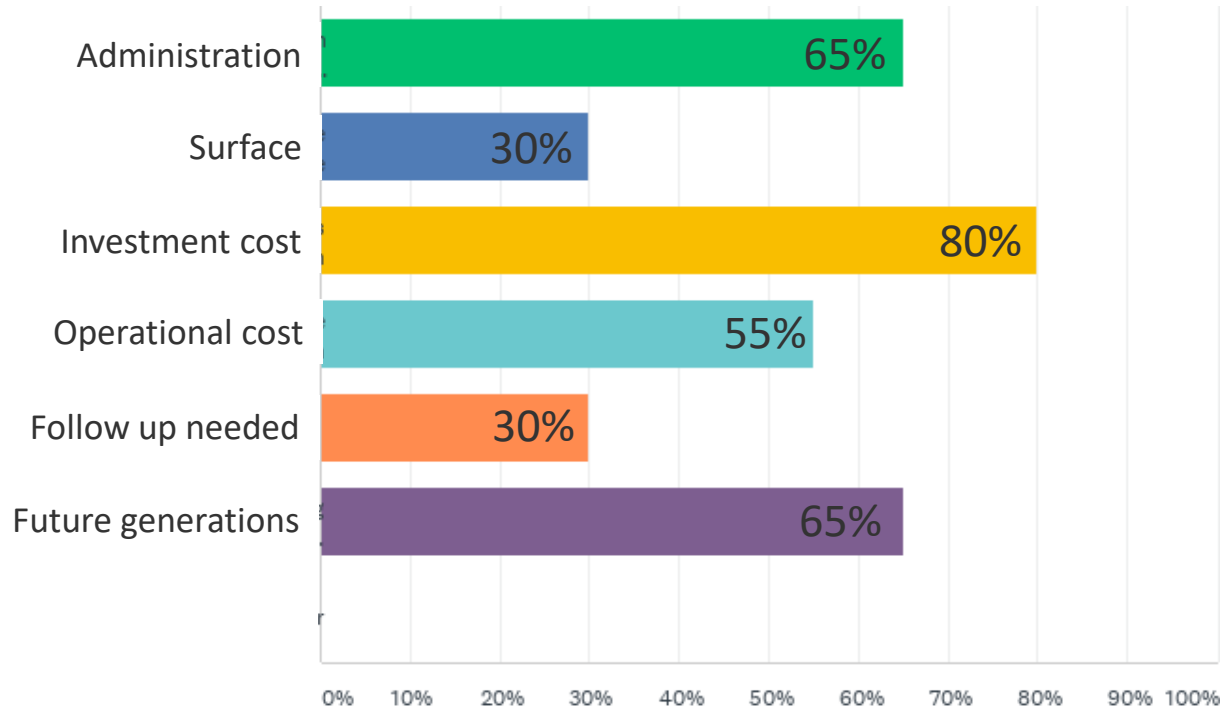
# Within which time frame would you consider this investment?

Beantwoord: 20 Overgeslagen: 9



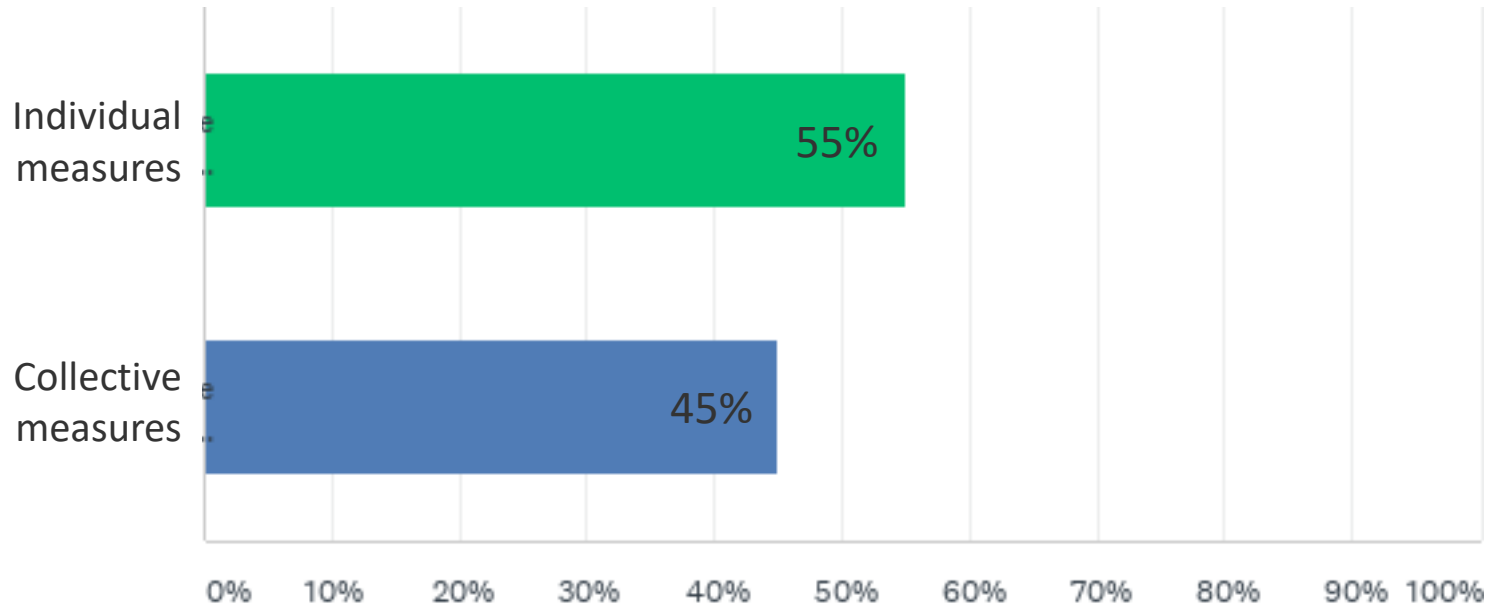
# Which factors influence your choice for a certain technology?

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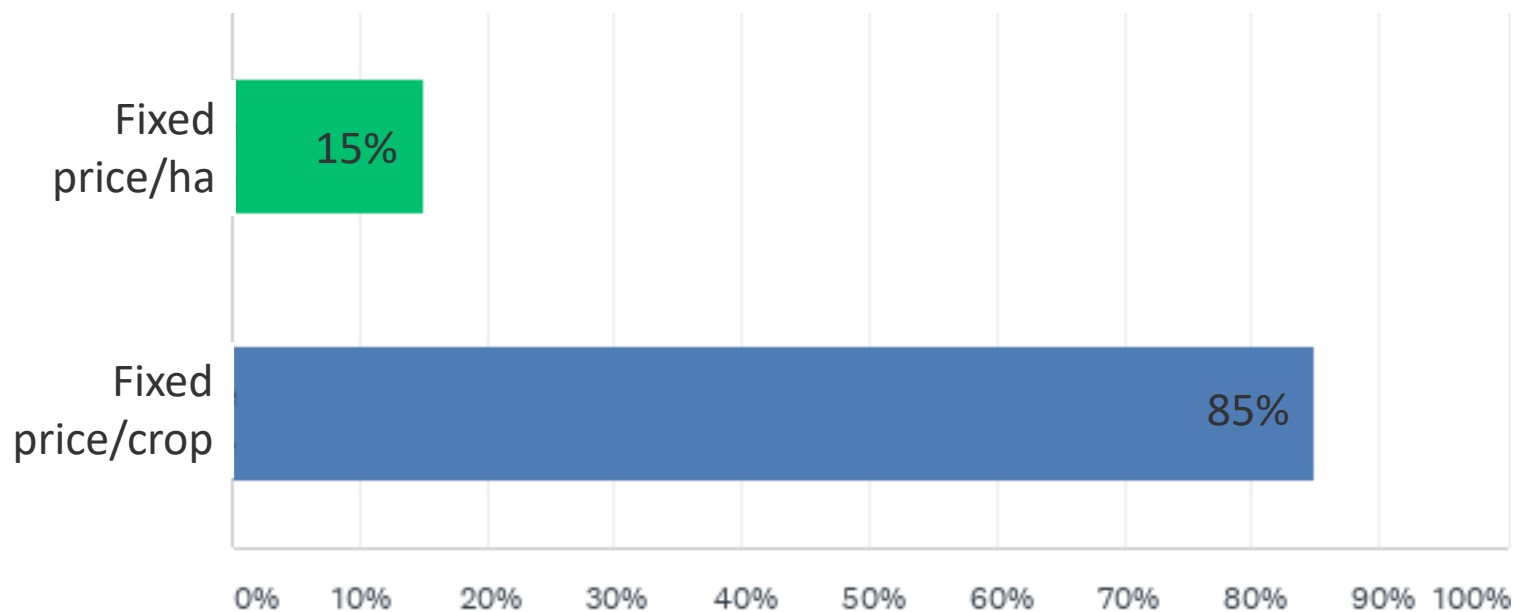
# I prefer:

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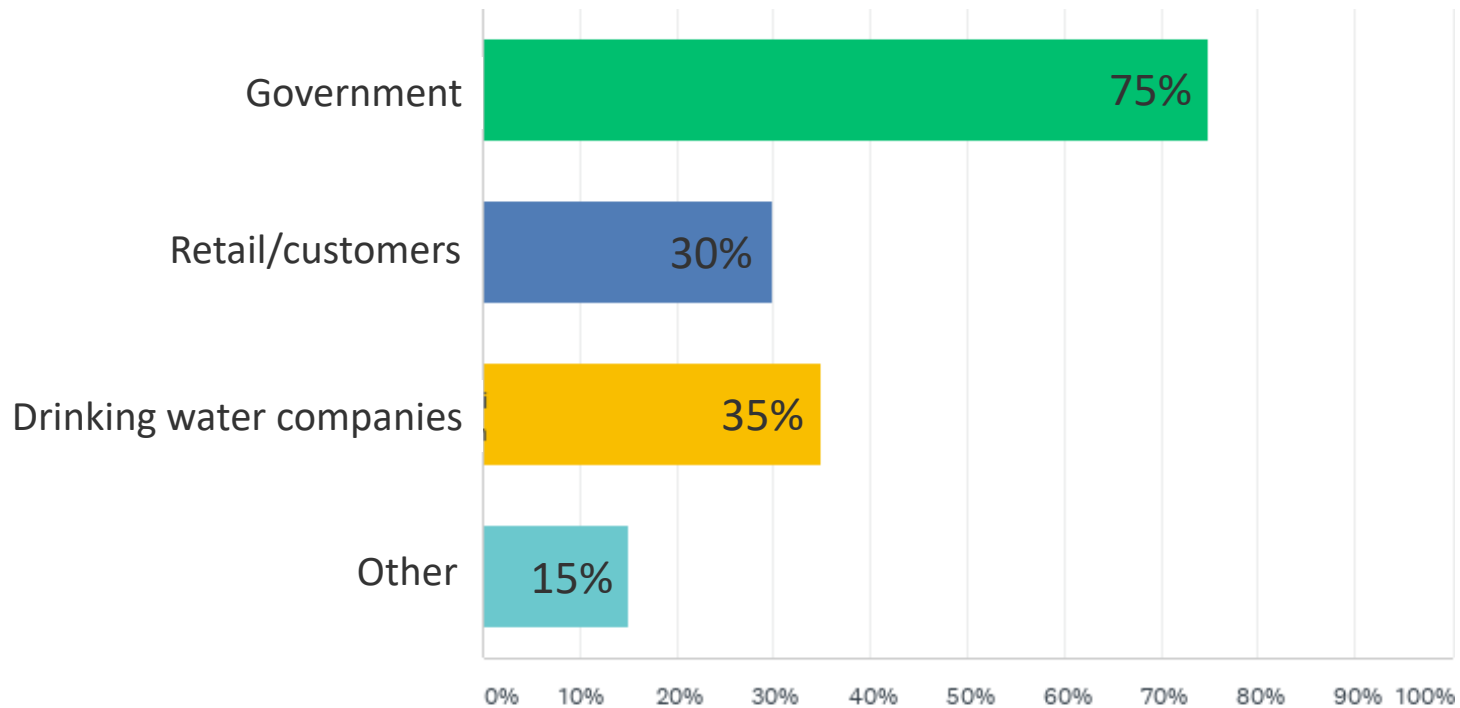
## In case of collective measures, which financing system is preferential?

Beantwoord: 20 Overgeslagen: 9



## In case of collective measures, who else should pay?

Beantwoord: 20 Overgeslagen: 9





# Farmers' opinion

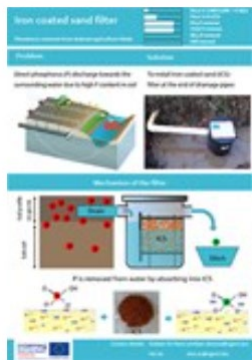
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- Simple technology required minimum of space
- Cost < € 5000
- Investments within 2-5 years
- Individual measures <-> collective measures
- Fixed price/crop

# Nuredrain information

- [NuReDrain, Interreg VB North Sea Region Programme](#)
- Scientific articles
- Filter fact sheets
- Videos
- MBBR manual: working principle, calculation tool, DIY build instruction

## Filter Fact Sheets



## Filter Construction Manuals



# Field visits with sun





# Field visits with rain





# Field tests in summer





# Field tests in winter





# Acknowledgements



**Interreg**  
North Sea Region  
European Regional Development Fund

